







COMESSA

COnstruction Mecanique Schiltigheim-Strasbourg SA















Outline

• Presentation of the Next-CSP project

- Modular Modelling Approach
 - Heliostat Field
 - Solar Receiver
 - Heat Exchanger
 - Gas Turbine

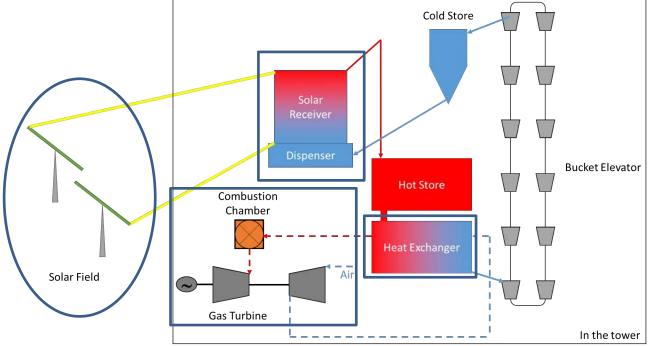


Results & Discussion



Next-CSP project

- Operation of the system
 - Solar Field
 - Dispenser
 - Tubular receiver
 - Hot and cold storage
 - Heat exchanger
 - **Bucket elevator**
 - Hybrid gas turbine



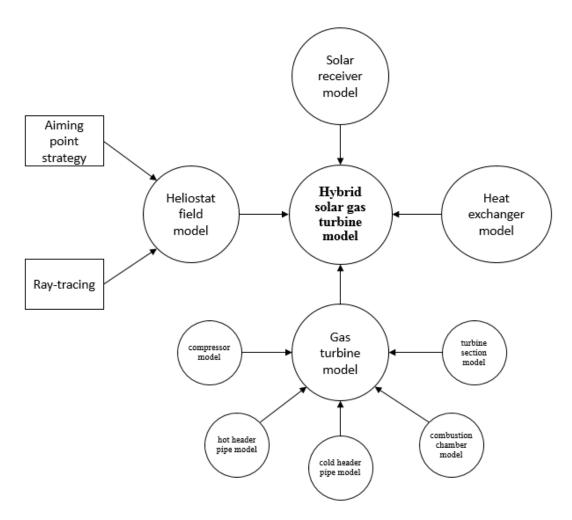
- Nominal Power (21st of March at noon):
 - on Receiver Aperture: ~3.8 MW
 - Transferred to the Particles in Solar Receiver: ~2 MW
 - Transferred to the Air: ~1.75 MW







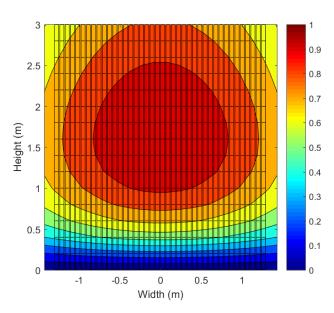
Modular Modelling Approach Global Vision





Heliostat Field

TABU search coupled with convolution-projection optical model Unizar



Objective normalized flux distribution

Horizontally ► Gaussian distribution

$$\phi_{inc} \le 500 \text{ kW/m}^2$$

Vertically $y = \left(\frac{x}{x_{peak}}\right)^{x_{peak}.b} exp\left(b(x_{peak} - x)\right)$

Number of aiming points = 25

3 m					
x	х	х	х	х	
х	х	х	х	х	
х	х	Х	Х	Х	1 60 cm
х	х	Х	Х	х	₩ 00 €111
х	х	Х	Х	х	

Cost function

Root-Mean-Square Deviation

Constraint

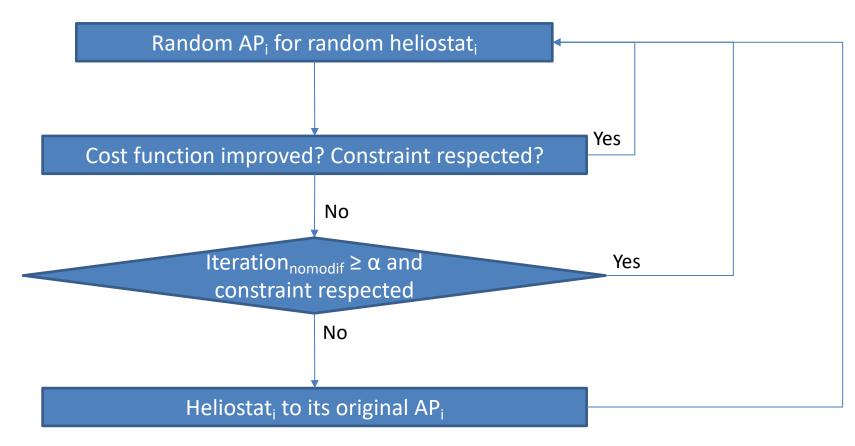
Not more than 30% of flux loss relative to base case





Heliostat Field

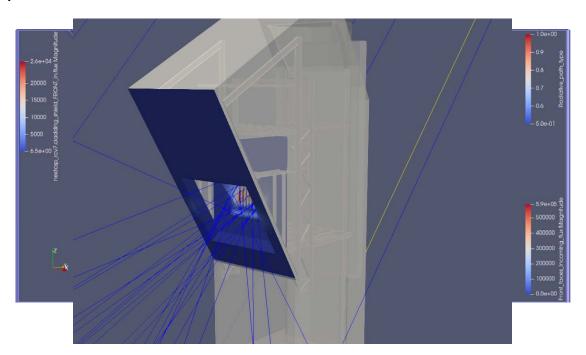
Algorithm





Heliostat Field

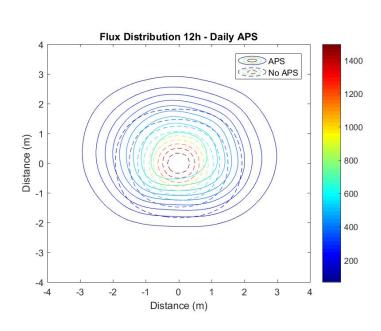
- Presentation of Solstice
 - New open-source ray-tracing software developed by the CNRS-PROMES laboratory and Meso-Star SAS
 - YAML (Yet Another Markup Language) language to create geometries
 - Import CAD model → Ray's path in complex geometry
 - Access to performance of the solar field



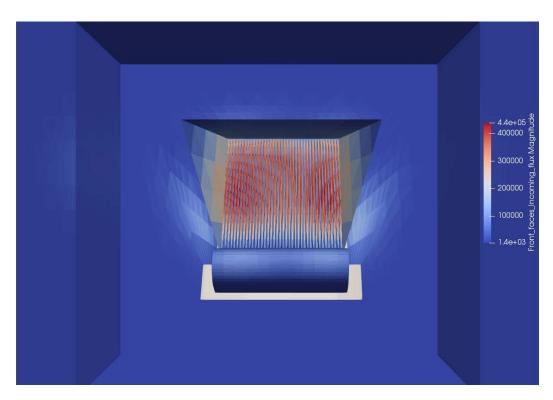


Heliostat Field

Typical Optical Results



TABU + Unizar



Solstice







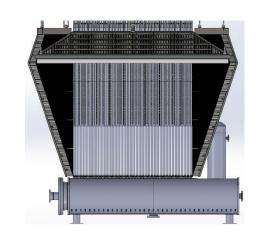
Modular Modelling Approach Solar Receiver

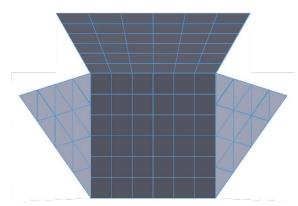
- Inputs from *Solstice*'s results
- 30 elements per tube (15 back of tubes, 15 front of tubes) → 1200 elements
- 104 elements for the cavity
- Visible from 0.3 to 3 μm carried out in Solstice and IR above 3 μm in thermal model
- Calculation of all the view factors
- Maximum Wall Temperature of 900°C
- Model Based on Net Radiation Method

$$\dot{Q}_i^{net} = A_i \cdot \left(\dot{\varphi}_i^{inc} + \sum_j F_{ij} \cdot J_j - J_i \right)$$

$$\dot{Q}_i^{res} = \dot{Q}_i^{net} - \left(\dot{Q}_i^{tr} + \dot{Q}_i^{loss}\right)$$

$$T_{i,t+dt}^{w} = T_{i,t}^{w} + \frac{\dot{Q}_{i}^{res} \times \Delta t}{m_{i}^{rec} \cdot c_{p}^{rec}}$$



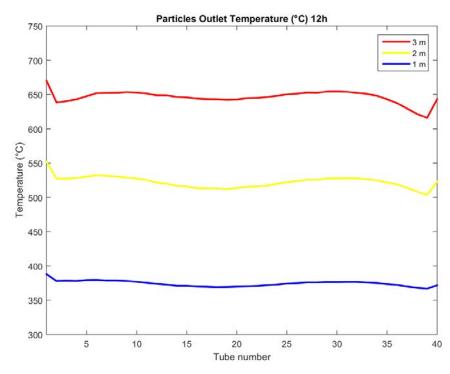






Modular Modelling Approach Solar Receiver

Typical Results



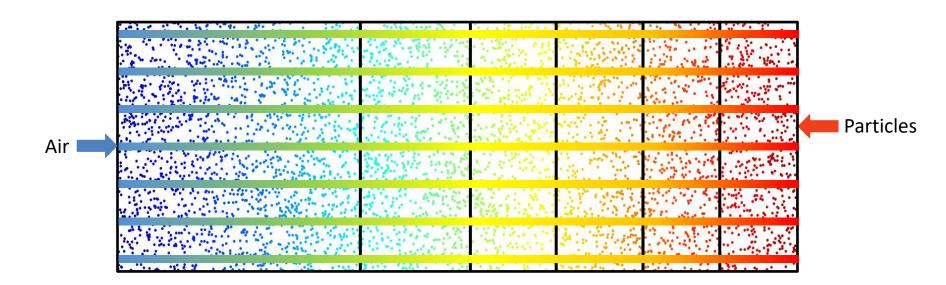
Maximum Temperature too high BUT possibility to decrease the number of operating heliostats





Heat Exchanger

- 6 stages Counter current
- Inputs from thermal model (Particles Inlet Temperature) and from gas turbine model (Air Inlet Temperature)



Input: design data Value for particle outlet temperature Value for air outlet temperature Value for tube temperature Heat transfer coefficient of air Conduction heat transfer in tubes Convection heat transfer in air No $Q_{air}^* = Q_{part}^{**}$ Yes Energy balance on the air No $Q_{air}^* = Q_{air}^{**}$ Yes Energy balance on the particles $Q_{part}^* = Q_{air}^{**}$ Yes Heat exchanger performance

Modular Modelling Approach Heat Exchanger

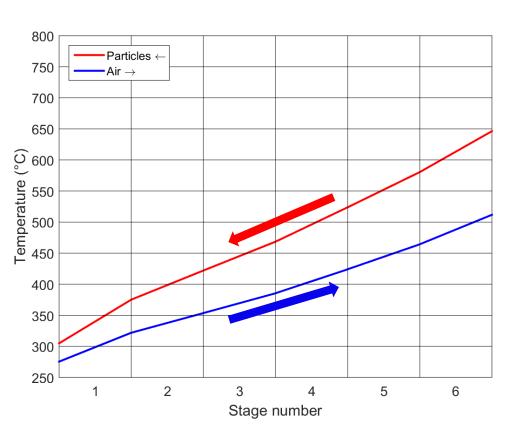
 $F_{friction} = (1.82 \times \log_{10}(Re) - 1.64)^{-2}$

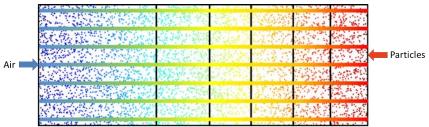
^(*) heat calculated based on heat transfer analysis, (**) heat calculated based on energy balance (inlet and outlet of the FB-HEX stage)



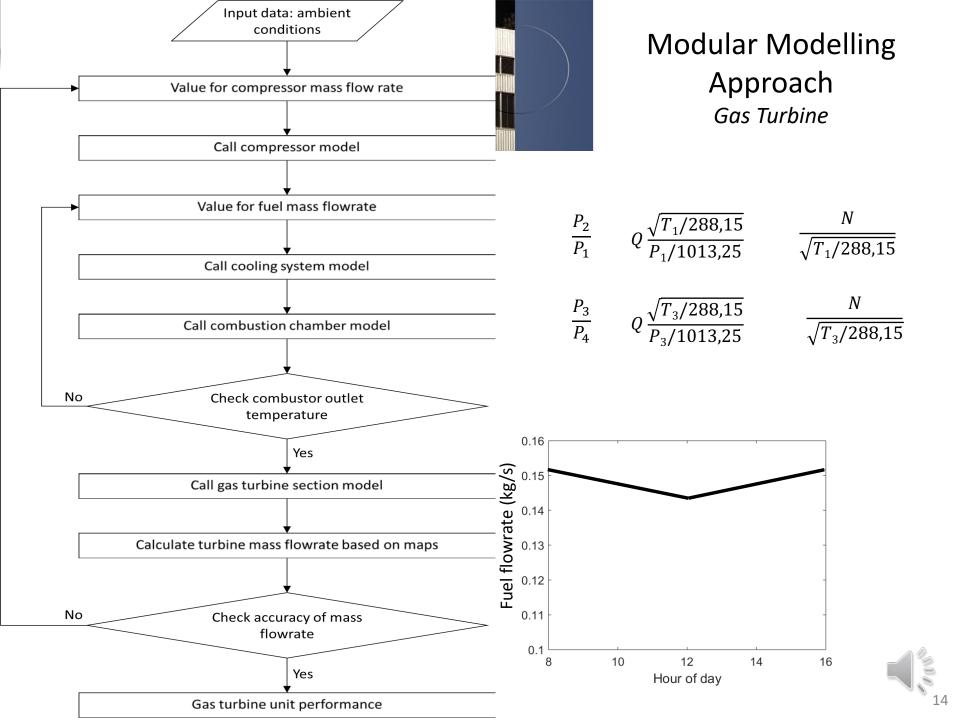
Heat Exchanger

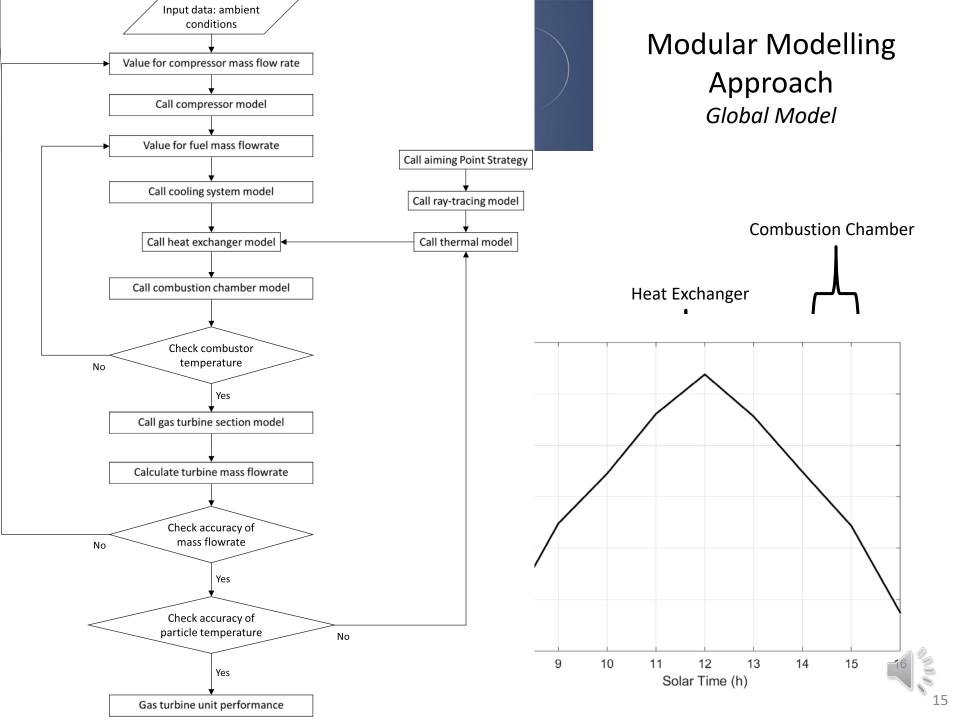
Typical Results





- The outlet gas temperature is limited by the heat transfer coefficient inside the tubes (air side)
- A better design is possible







Discussion

- Low solar share BUT can be increased with:
 - Better heat transfer wall/particles in receiver
 - Better HEX design
 - Optimized solarized turbine (current one is off-the-shelf)
- Major objectives of this project is to gain experience in the particle solar loop and in the hybridisation





Thank you for your attention Any Questions?

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