

Comparison of Simulated and Measured Flux Distributions at the Aperture of the Next-CSP Solar Receiver

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COMESSA
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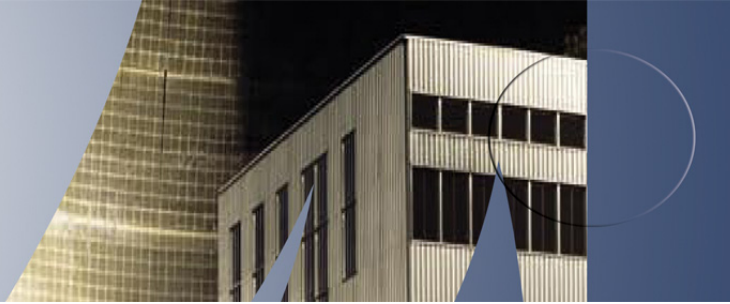
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Outline

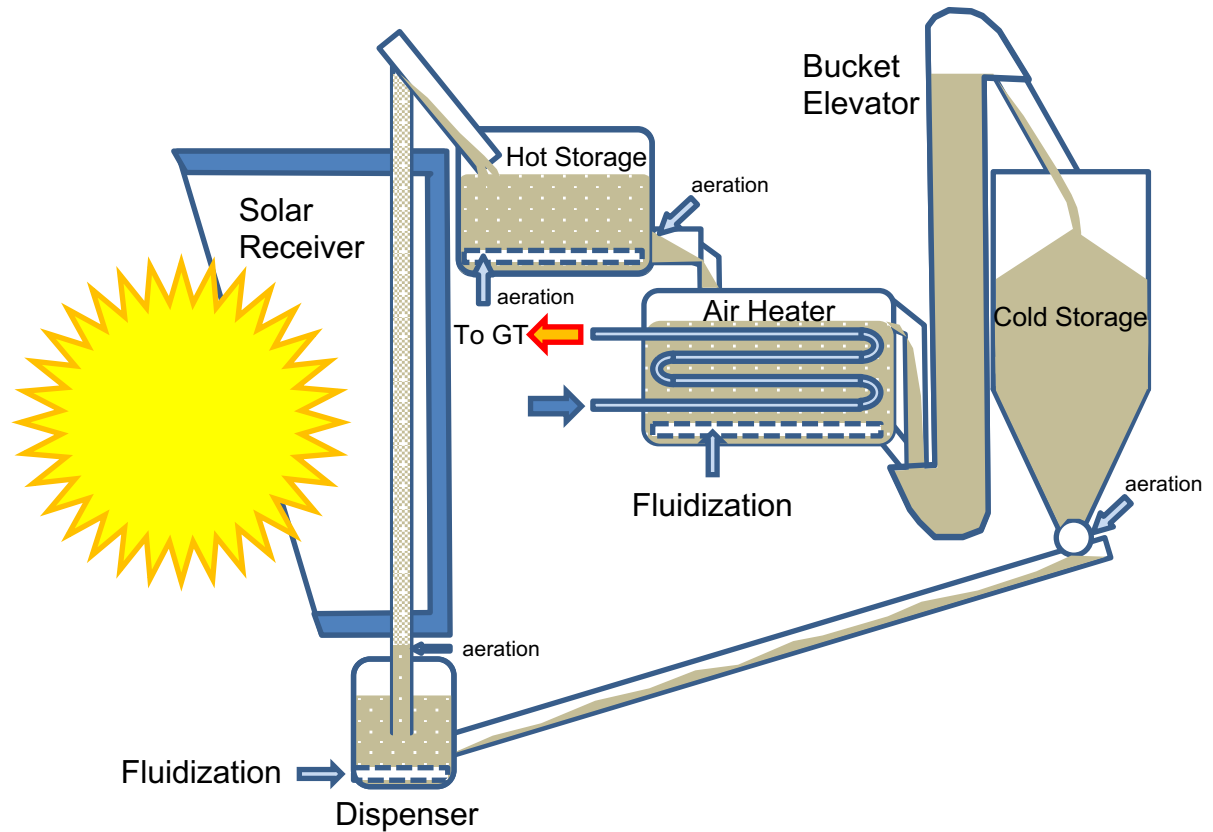
- Presentation of the Next-CSP Project
- Description of the Solar Receiver
- Methodology
 - TABU Search/*Solstice*
 - Heat Flux Measurement
- Results & Perspectives





Next-CSP project

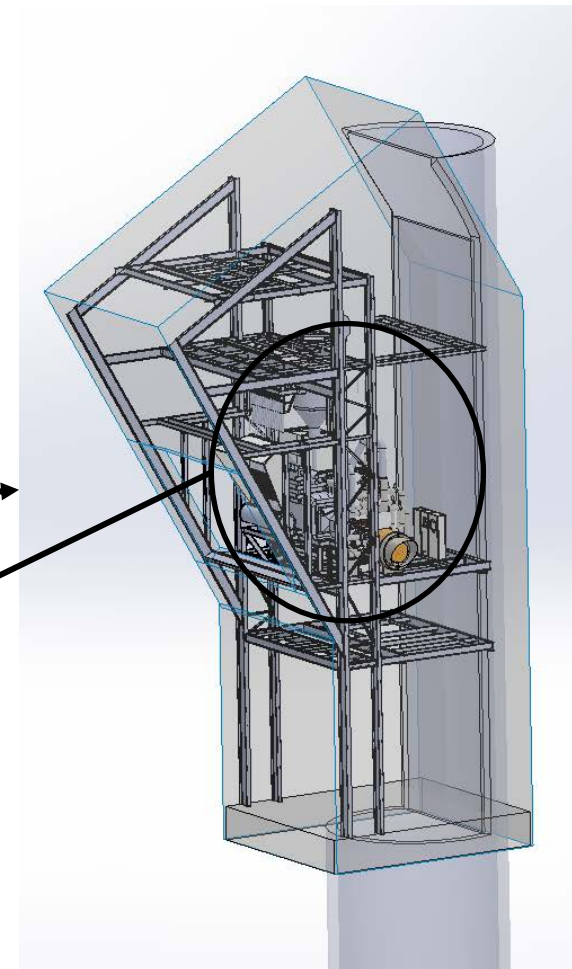
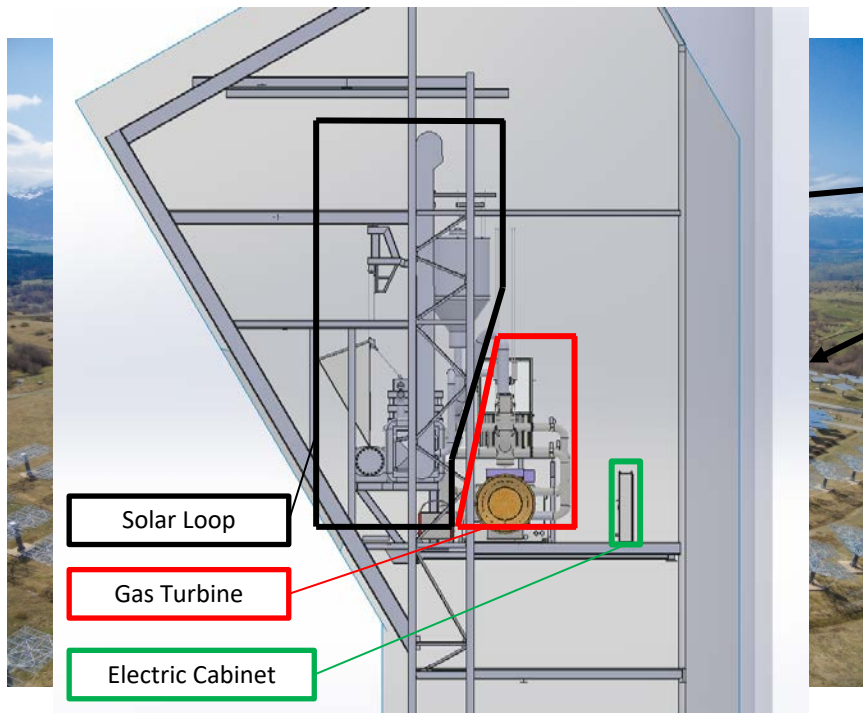
- Operation of the system
 - Dispenser
 - Tubular receiver
 - Hot and cold storage
 - Air heater
 - Bucket elevator
 - Hybrid gas turbine

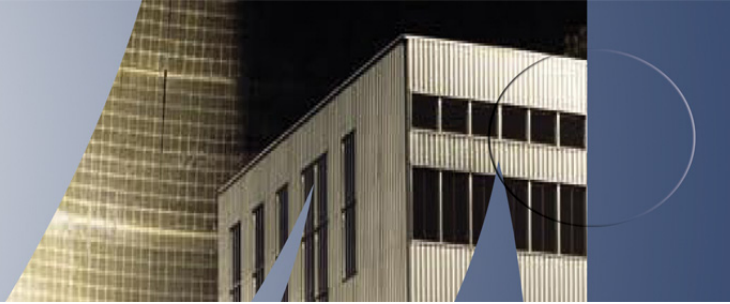




Next-CSP project

- Installation at the Themis site
 - Tower of 104 m
 - 107 heliostats of 54 m² each
 - System between 83 m and 92 m height
 - ~70 tons



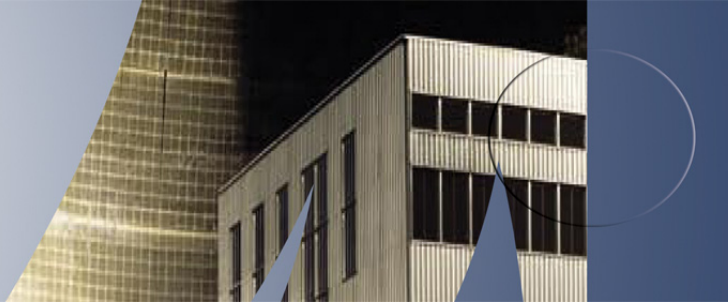


Next-CSP project

- Major challenges
 - **Develop a solar receiver able to heat particles up to 700°C**
 - Design and test a two-tank particle thermal energy storage and a particle-to-pressurized air heat exchanger.
 - Integrate a hybrid gas turbine with the solar loop.
- Major barriers
 - Heat transfer limitation
 - **High temperature materials**
 - Particle conveying and circulation in a close loop
 - Control of the complete system

Aiming point strategy on the Next-CSP receiver

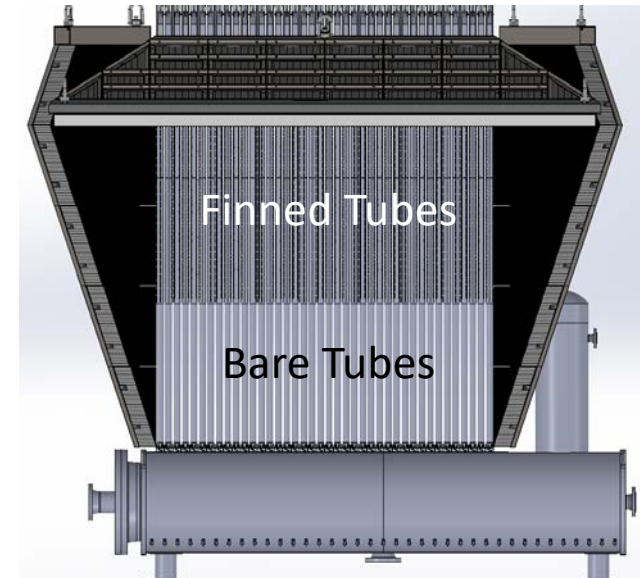




Description

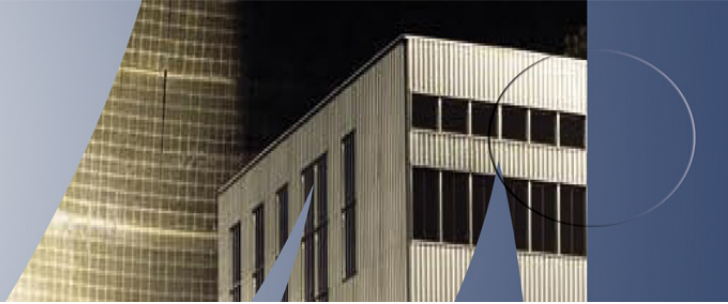
- Tubular receiver (SS 310S) with back refractory panel
- 40 tubes - 1 m bare (lower part) and 2 m finned
- Divergent half cavity made of refractory panels
- Refractory panels → ALSIFLEX®-1260
- Angles of the cavity panels comes from position of most Eastern, Western and Northern heliostats

→ Complex geometry and optical paths



Aiming point strategy has to take into account the complex geometry

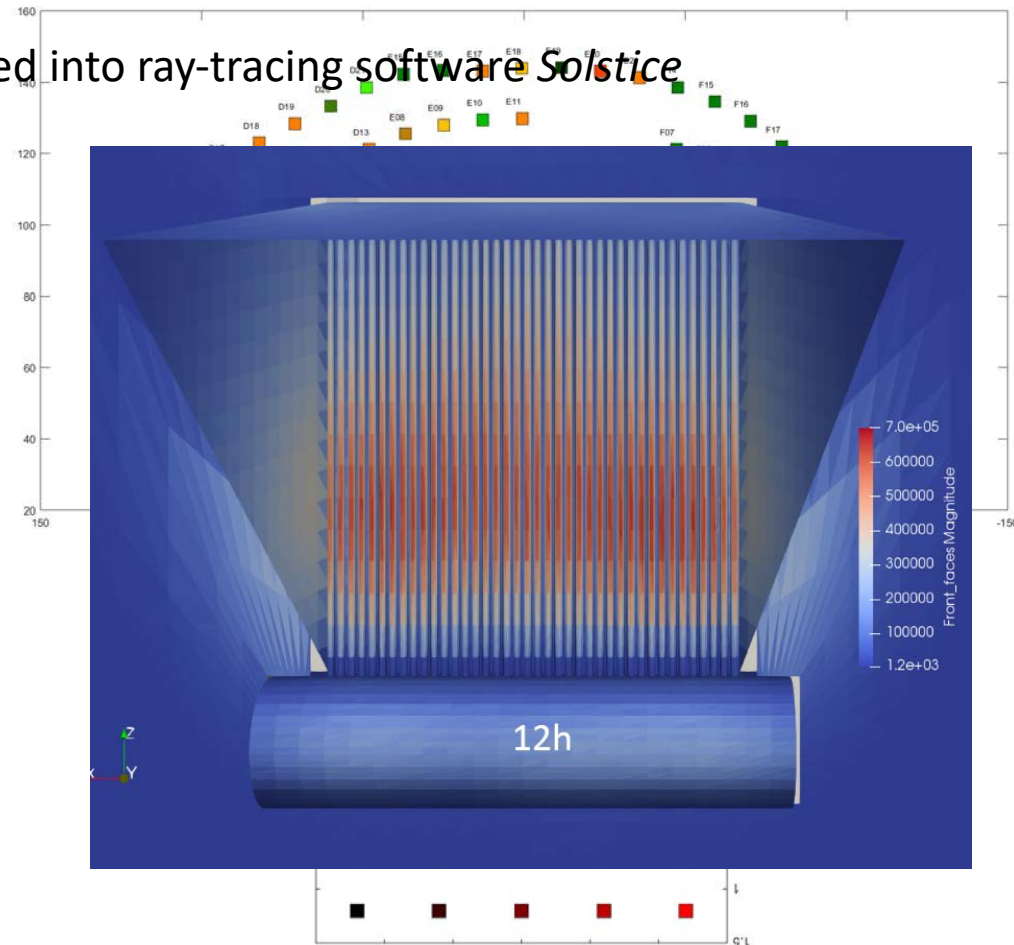


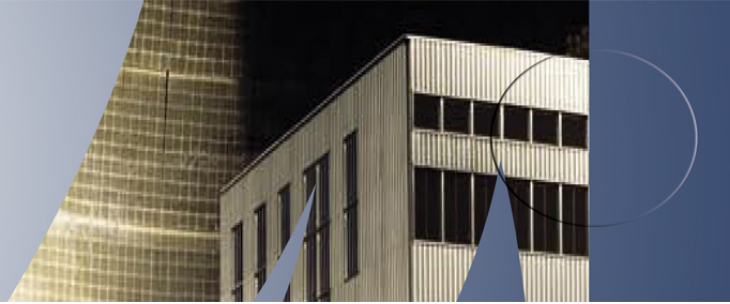


Methodology

Simulation Tools

- TABU search coupled with convolution-projection optical model Unizar
- Results introduced into ray-tracing software *Soltice*

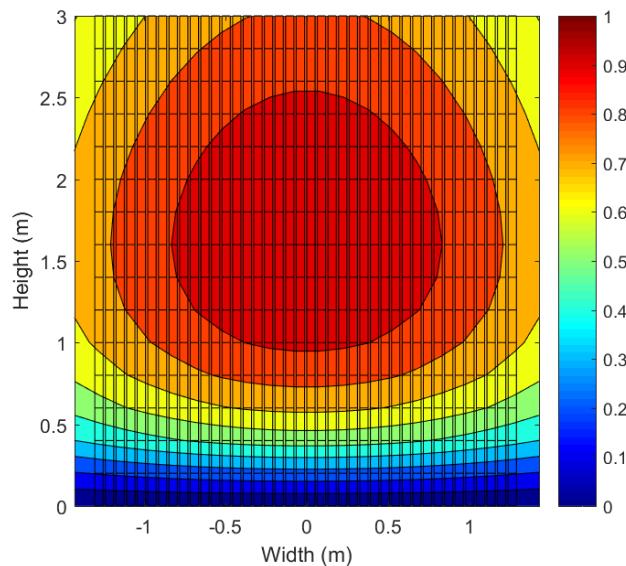




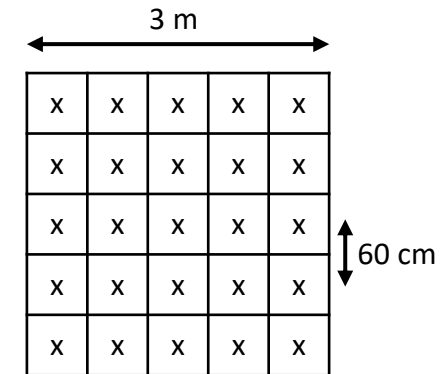
Methodology

TABU Search

- Definition of objective normalized flux distribution, # of aiming points, cost function and constraint



Number of aiming points = 25



Cost function

Root-Mean-Square Deviation

Constraint

Not more than 30% of flux loss relative to base case

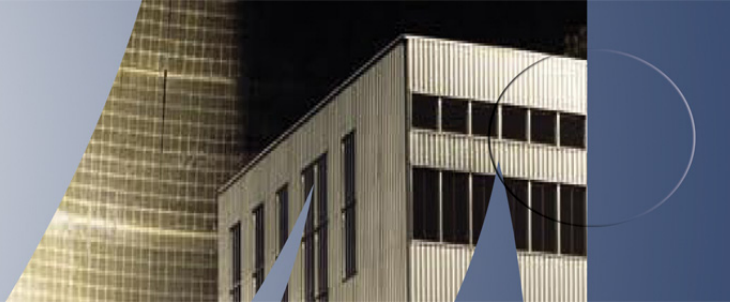
Objective normalized flux distribution

Horizontally → Gaussian distribution

Vertically → $y = \left(\frac{x}{x_{peak}} \right)^{x_{peak} \cdot b} \exp(b(x_{peak} - x))$

$$\Rightarrow \phi_{inc} \leq 500 \text{ kW/m}^2$$

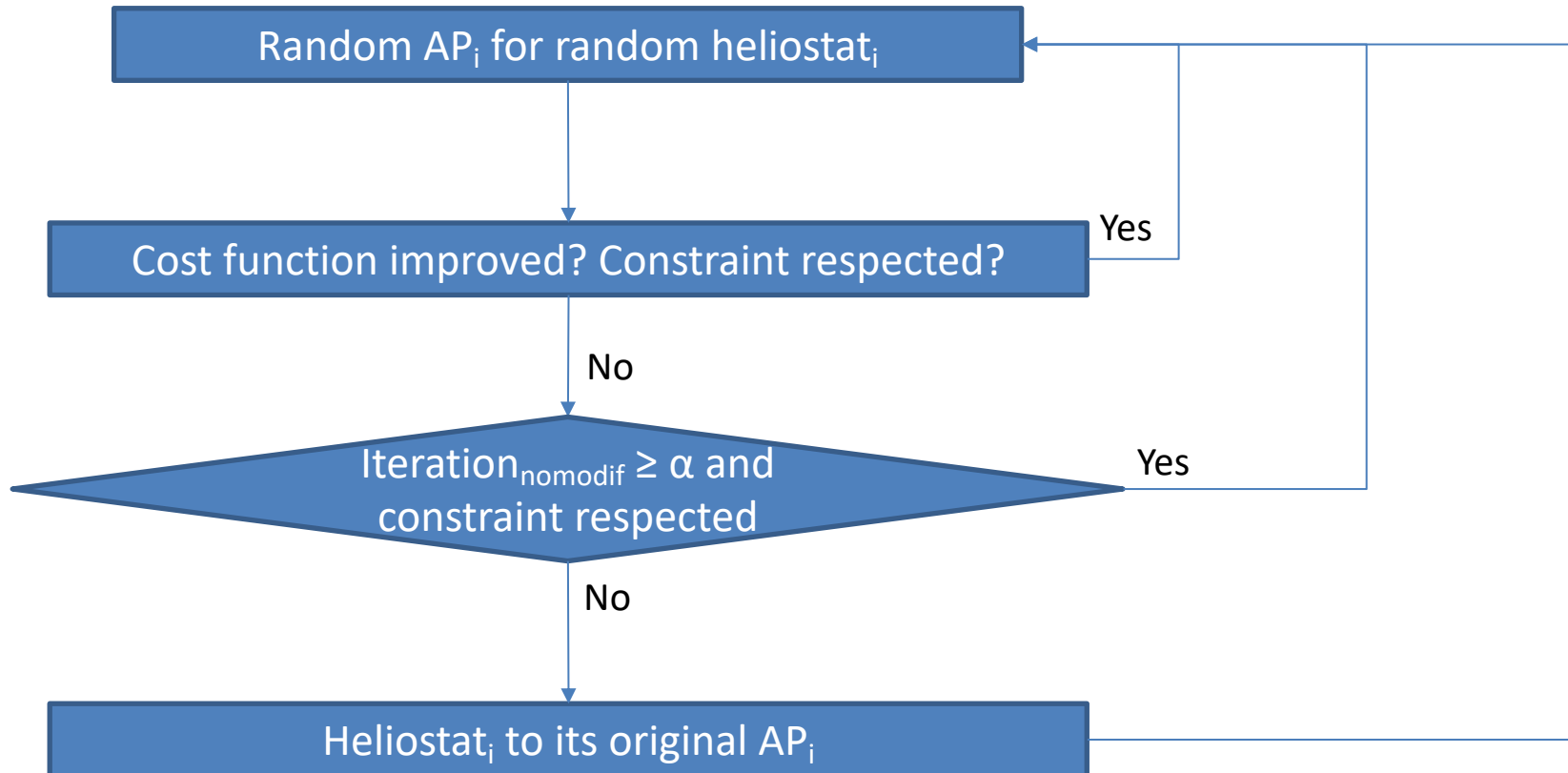




Methodology

TABU Search

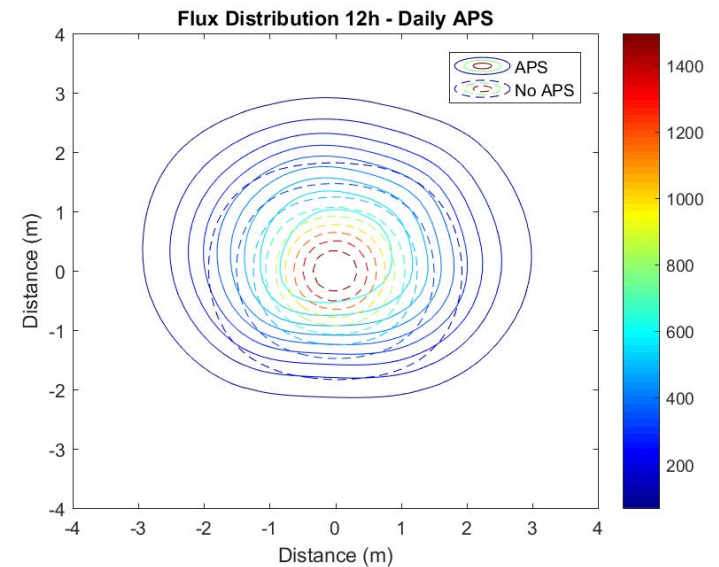
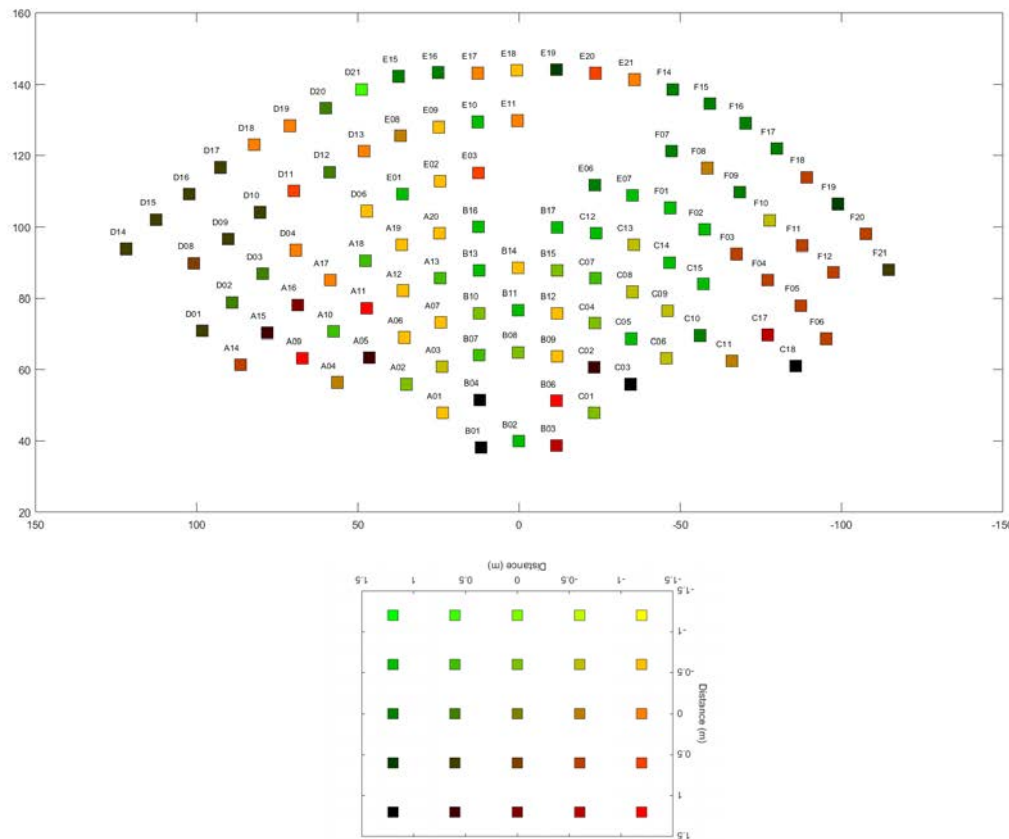
- Algorithm

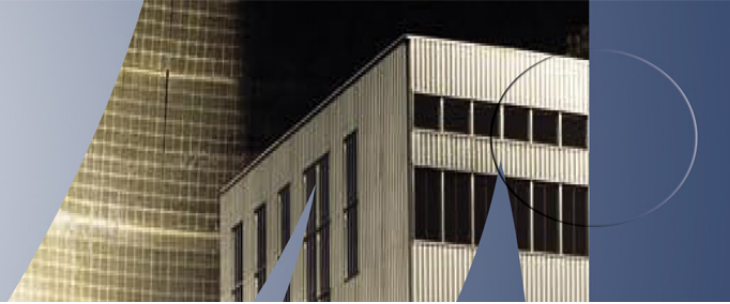


Methodology

TABU Search

- Typical results

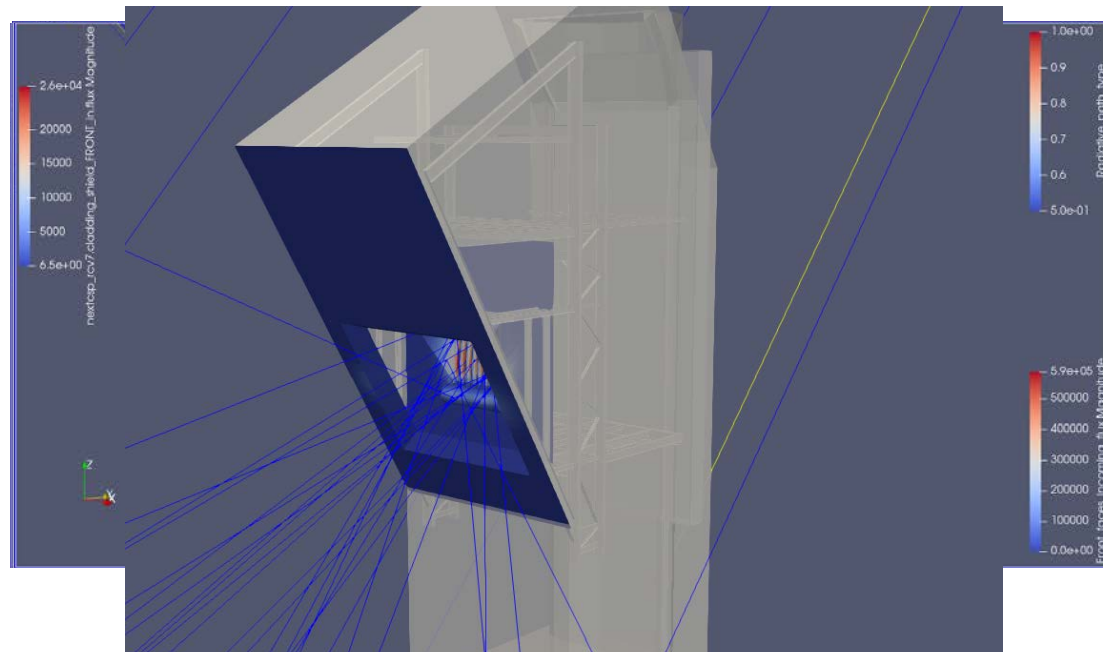


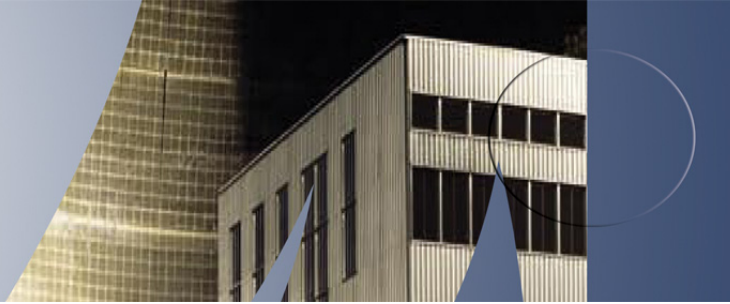


Methodology

Solstice

- Presentation of *Solstice*
 - New open-source ray-tracing software developed by the CNRS-PROMES laboratory and Meso-Star SAS
 - YAML (Yet Another Markup Language) language to create geometries
 - Import CAD model → Ray's path in complex geometry
 - Access to performance of the solar field

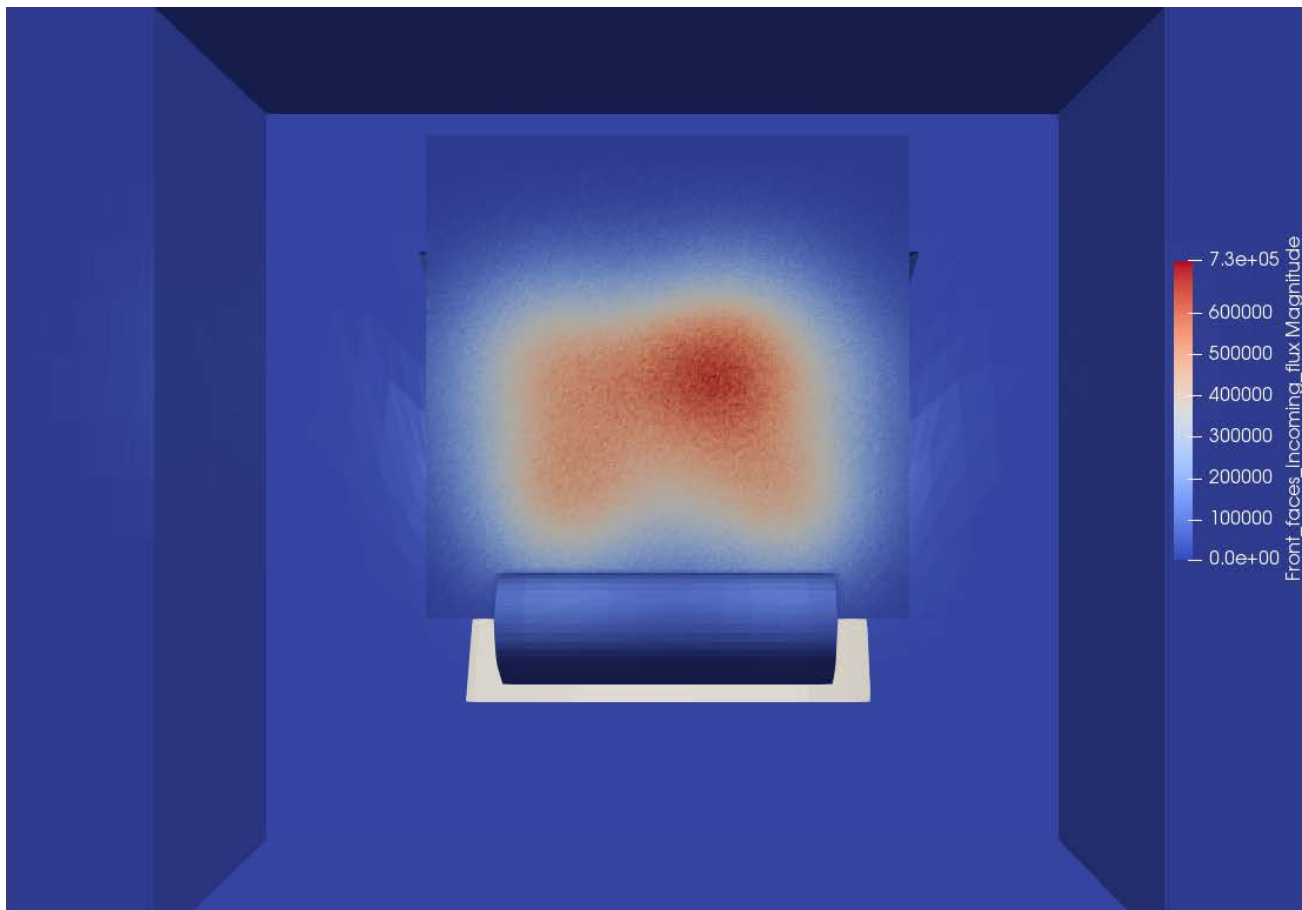


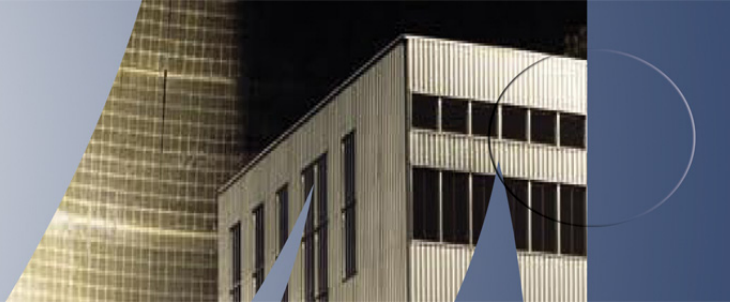


Methodology

Solstice

- Flux distribution on the scanning bar plane with a virtual target

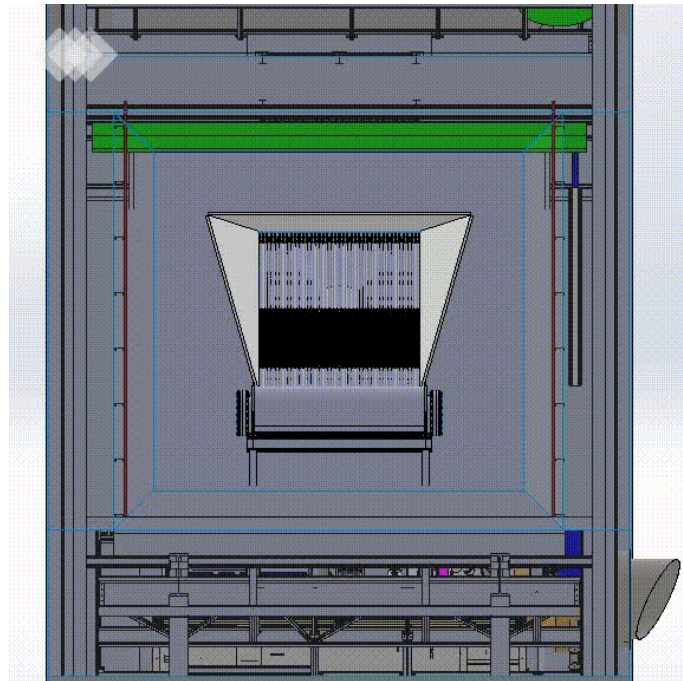


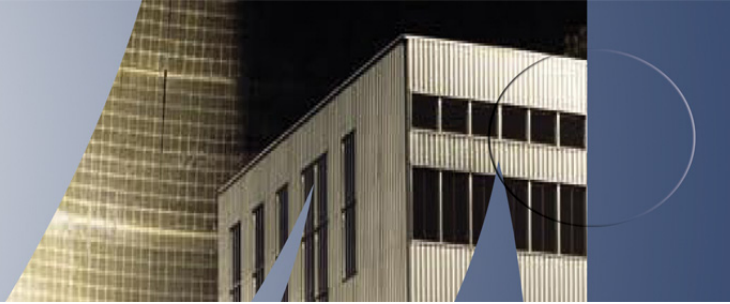


Methodology

Flux Measurement System

- Consists in:
 - CMOS camera
 - Heat flux sensor
 - Scanning bar
- Measure the heat flux distribution at the aperture of the receiver

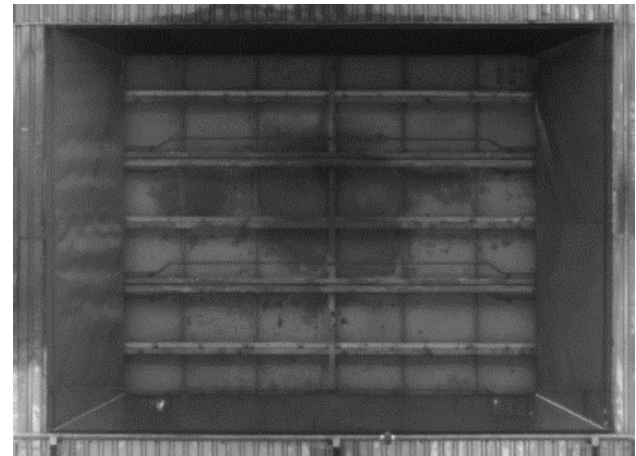




Methodology

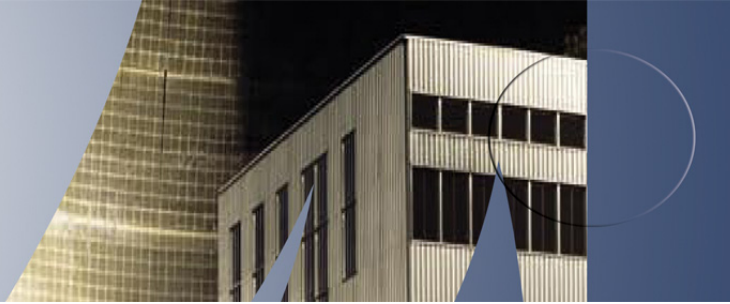
Flux Measurement System

- CMOS camera installed in the solar field



- Basler, sensor CMOS Sony IMX174, 1920*1200, monochrome
- High picture frame rate (up to 163 FPS)
- 16-bit dynamic
- Pixel of 2.34 x 2.34 mm

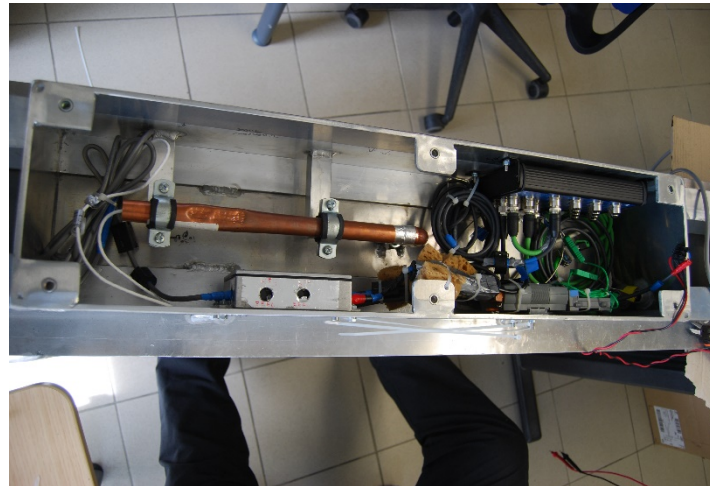




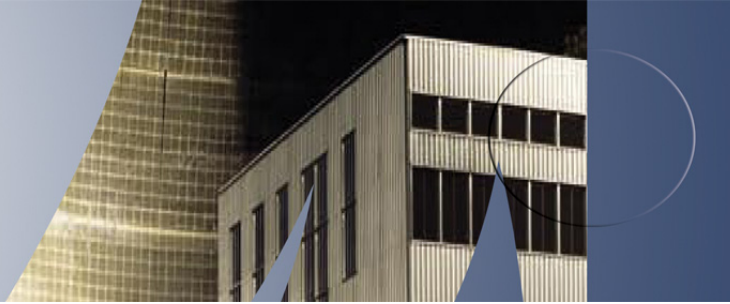
Methodology

Flux Measurement System

- Heat flux sensor installed on the scanning bar



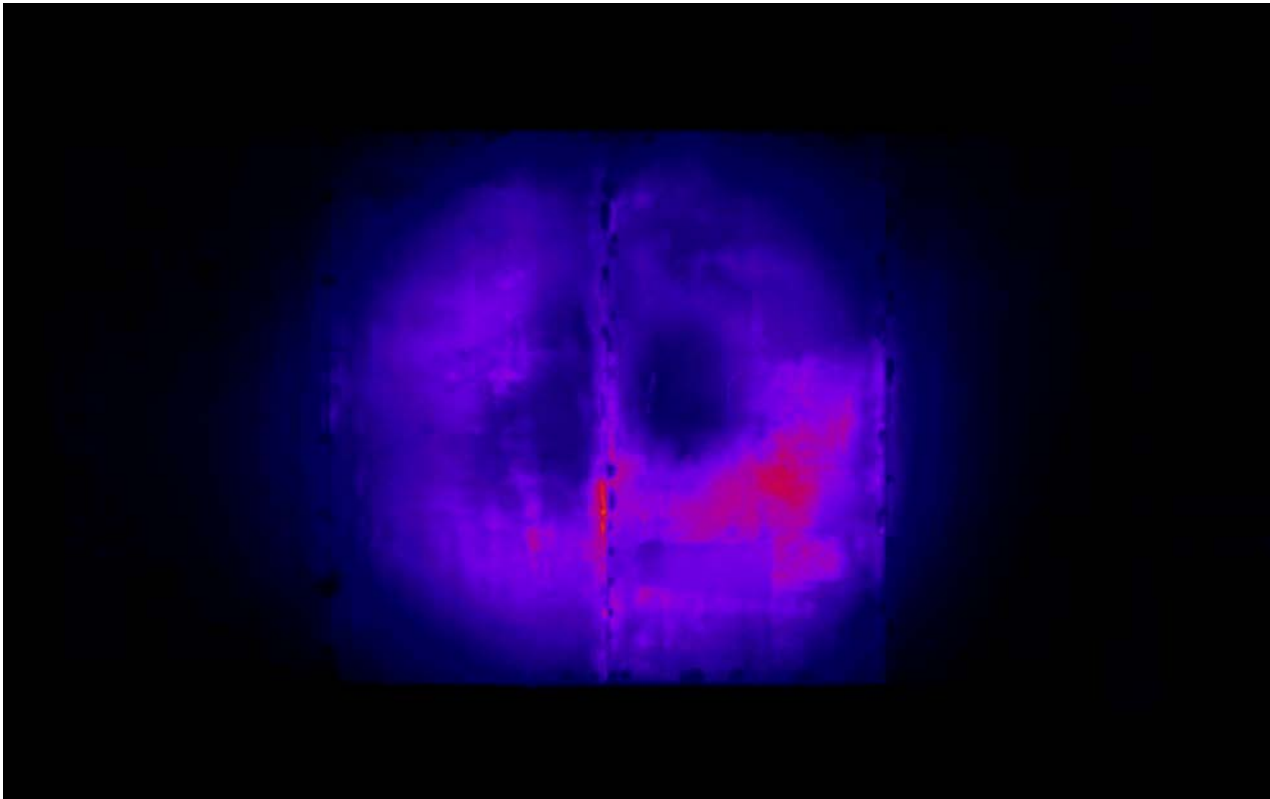
- Heat flux micro-sensor model HFM 6
- 17 to 300 μ s response time
- Thermopile 4 mm in diameter, covered with Pyromark[®] film $\rightarrow \alpha = 94\%$
- Accuracy of $\pm 3\%$
- High-speed A/D converter and data acquisition system ADDI DATA MSX-E3011

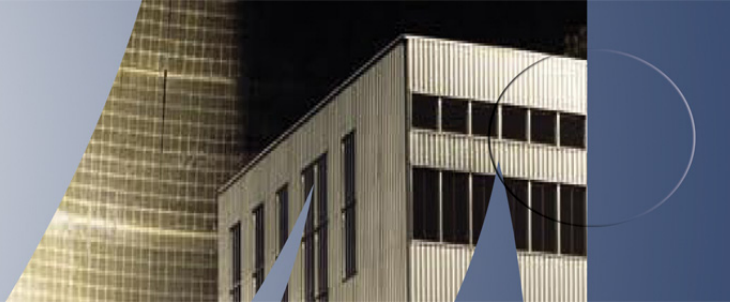


Methodology

Flux Measurement System

- View of the scanning bar from the CMOS camera





Methodology

Flux Measurement System

- Data processing
 - Flat-field correction

$$I_{net} = \frac{I_{raw} - I_{black}}{I_{flat} - I_{black}}$$

- Peak Signal to Noise Ratio (PSNR)

$$PSNR = 10 \log_{10} \left(\frac{1}{rms(I_{raw} - I_{net})} \right)$$

- Background subtracted from each “net” image

$$I_{corr} = I_{net} - I_{back}$$





Methodology

Flux Measurement System

- Data processing
 - Spatial derivative approach to detect the bar

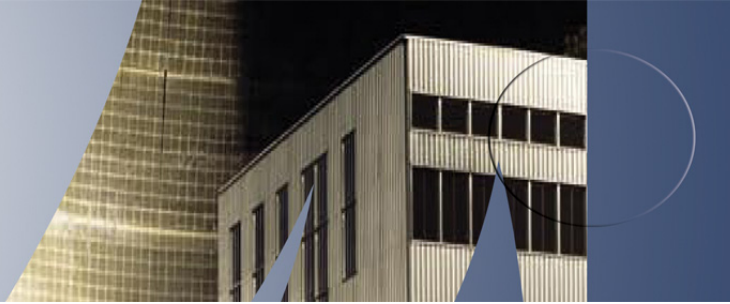
$$I_{corr-n} = 2 \frac{I_{corr} - Min_{pix-all}}{Max_{pix-all} - Min_{pix-all}} - 1$$

$$I_{grad-x} = grad(I_{corr-n})$$

$$I_{grad-x-n} = 2 \frac{I_{grad-x} - Min_{grad-x-all}}{Max_{grad-x-all} - Min_{grad-x-all}} - 1$$

$$Mean_{grad-x-n} = mean_y(I_{grad-x-n})$$

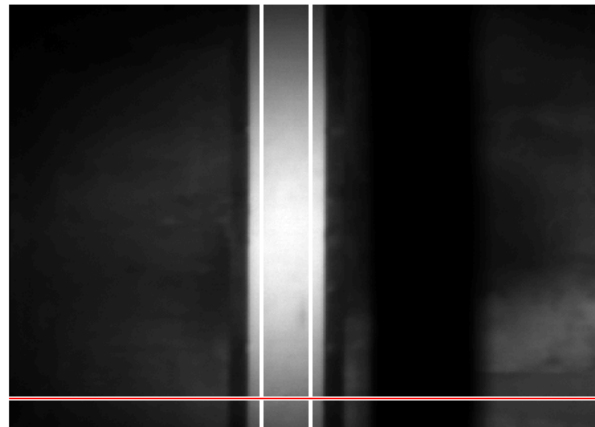
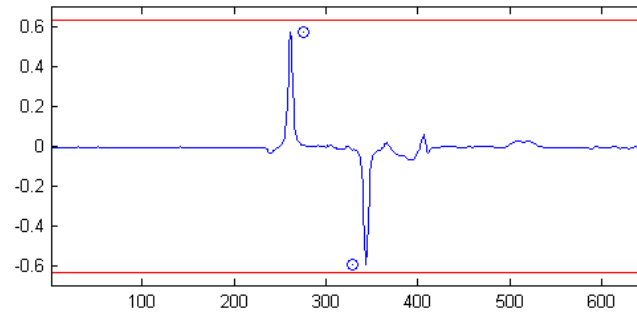




Methodology

Flux Measurement System

- Data processing
 - Spatial derivative approach to detect the bar





Methodology

Flux Measurement System

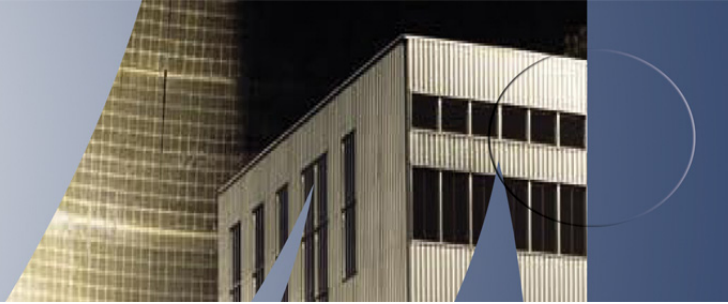
- Data processing
 - Mapping grey value

$$MeanValPixel(p) = \frac{1}{n} \sum_{i=1}^n ValPixel_p(i)$$

$$STD(p) = \frac{1}{n} \sqrt{\sum_{i=1}^n [ValPixel_p(i) - MeanValPixel(p)]^2}$$

- $ValPixel_p(i)$ that deviate from the average by more than twice the $STD(p)$ are rejected

$$MeanValPixel(p) - 2 \times STD(p) < ValPixel_p(i) < MeanValPixel(p) + 2 \times STD(p)$$



Methodology

Flux Measurement System

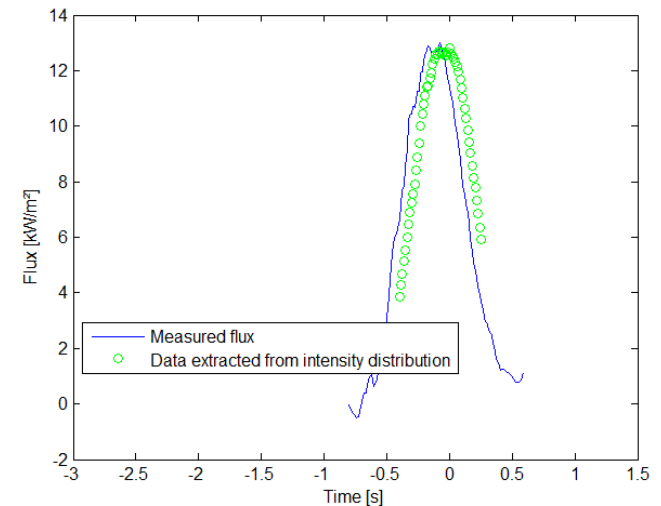
- Data processing

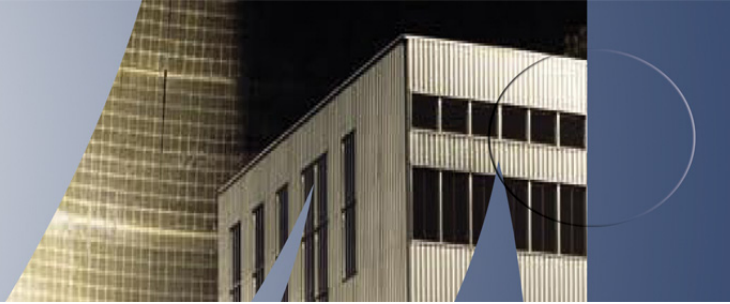
- Calibration

$$\begin{cases} X_{flux}(n) = X_{max}(n) + dF_x \\ Y_{flux} = dF_y \end{cases}$$

- $ValPixel(x_n) = ValPixel(X_{flux}(n), Y_{flux})$

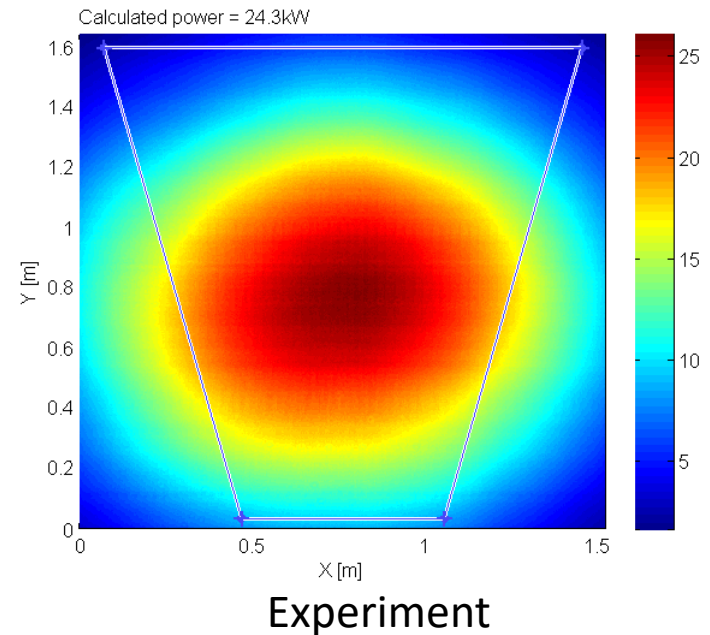
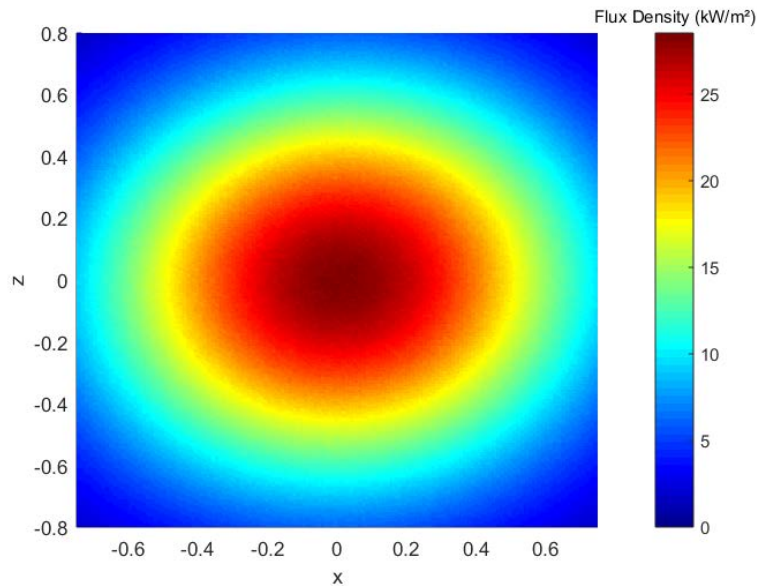
- Power calculation: $P_{solar-in} = \sum_{cells} [Flux(cell_i) \times Area(cell_i)]$





Results & Perspectives

- Single Heliostat



- Comparison with an APS with more heliostats when operating the solar loop



Thank you for your attention

Any Questions?

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